

Hf Doping of an Aluminide Bond Coat for Single Crystal Jet Engine Turbine Blades

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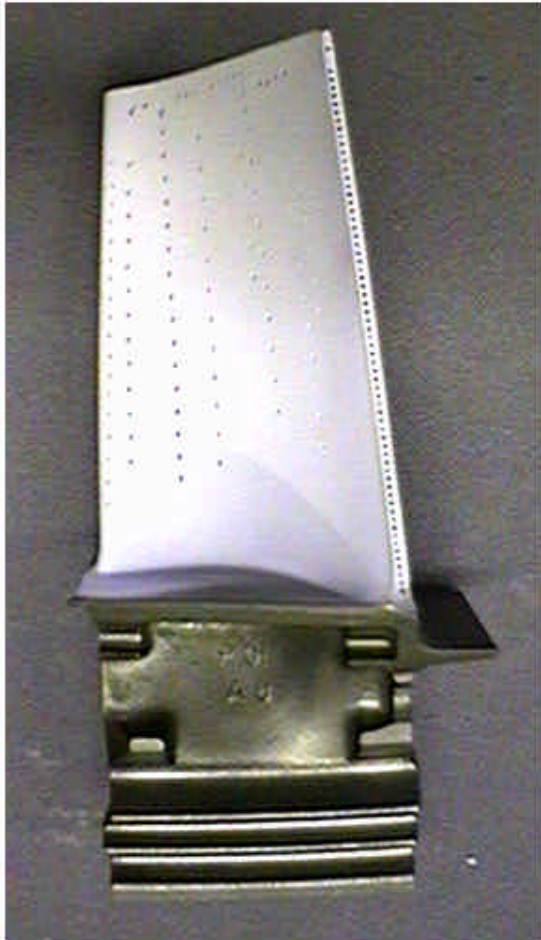
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Summary of Efforts

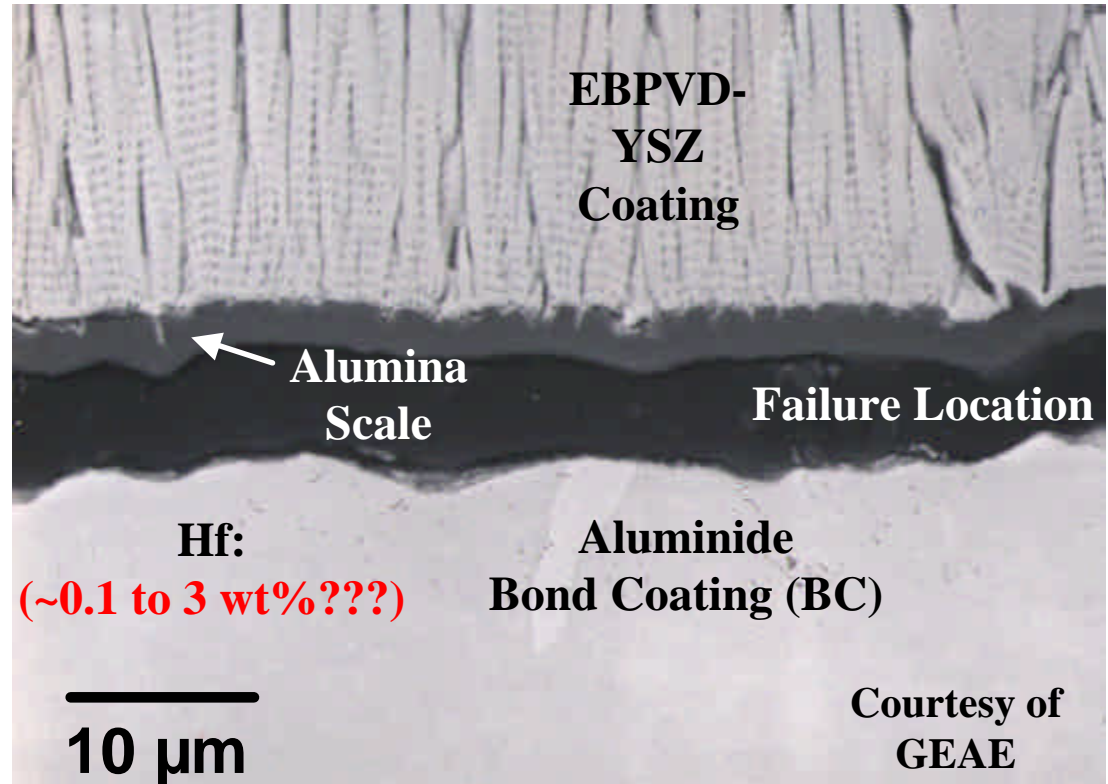
Thermal barrier coatings (TBCs) are currently used, in conjunction with air cooling, to prolong the life of metallic "hot-section" Ni-based superalloy components used in aircraft engines and power generation turbines with an annual market size of ~\$1.5 billion. The advent of next-generation TBCs requires superior oxidation characteristics over those of current metallic bond coatings. One potent way of improving oxidation resistance is to dope Ni-based alloys with a small amount of a reactive element such as Y, Hf, or Zr. We have performed Hf doping experiments while the surface of a single crystal Ni alloy was being aluminized to form an aluminide (β -NiAl) coating matrix by chemical vapor deposition for improved oxidation resistance of the NiAl coating.

A continuous doping procedure, in which HfCl_4 and AlCl_3 were simultaneously introduced with H_2 , required a high $\text{HfCl}_4/\text{AlCl}_3$ ratio ($>\sim 0.6$) to cause the precipitation of Hf-rich particles ($\sim 0.1 \mu\text{m}$) at grain boundaries of the coating layer with the overall Hf concentration of ~ 0.05 to $0.25 \text{ wt}\%$. Below this ratio, Hf did not incorporate as a dopant from the gas phase as the coating matrix appeared to be "saturated" with other refractory elements partitioned from the alloy substrate. We have also studied a sequential doping procedure that consists of pretreating the alloy surface with HfCl_4 and H_2 followed by aluminizing. The Ni alloy surface reacted significantly with HfCl_4 and H_2 , even for a short exposure of 30 seconds, to form an Hf-rich layer containing $\text{Hf}_8\text{Ni}_{21}$, Hf_3Ni_7 , and HfNi_3 precipitates. This Hf-rich layer apparently worked as a diffusion barrier to mitigate the columnar growth of β -NiAl grains. Our results suggest that the most promising avenue for controlling Hf concentration and distribution is to periodically nucleate very small Hf particles in the coating matrix via time-resolved switching between AlCl_3 and HfCl_4 precursors.

Superior Adhesion Needed for Next Generation TBCs



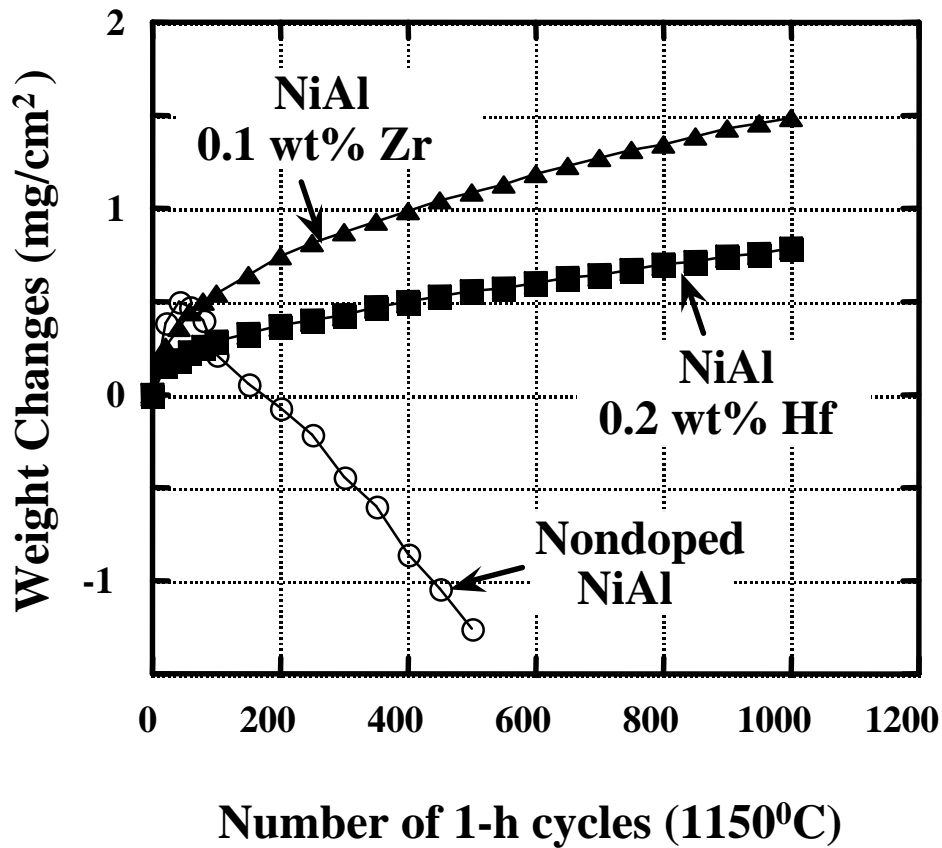
Single crystal Ni super alloy with TBC



Problems observed in industry

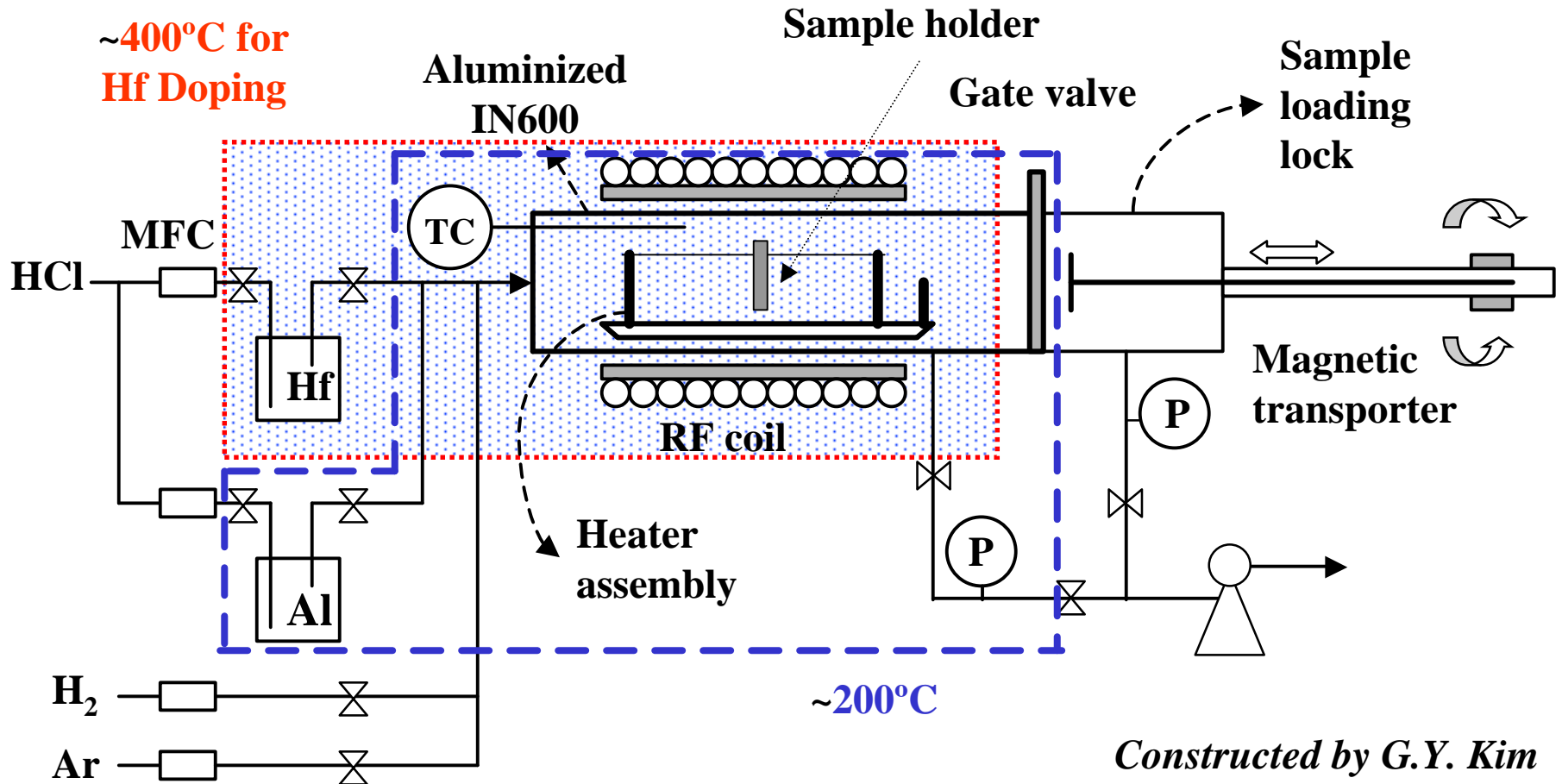
- Lack of process reproducibility
- Inconsistent composition/performance relationships

“Model” TGO Behavior

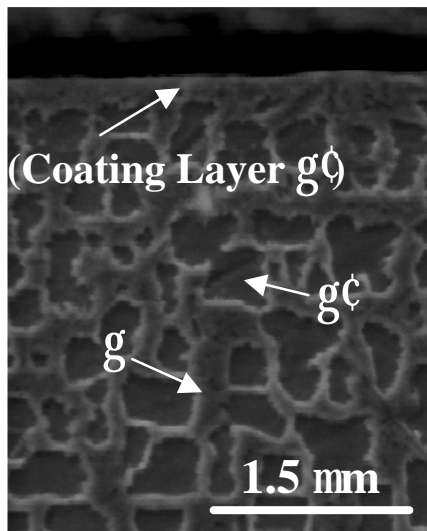


- **Cast stoichiometric b-NiAl**
 - Pint et al., 1998
- **Beneficial effects of Hf**
 - TGO growth kinetics
 - Columnar TGO
 - Immobilized sulfur impurity
 - Creep resistance of b-NiAl
- **Optimum performance**
 - ~0.2 wt% Hf
- **Hf solubility in cast b-NiAl**
 - Not precisely measured
 - Estimated ~0.1 wt% by Pint

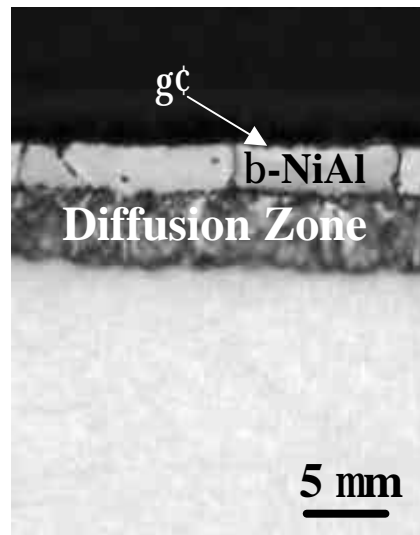
CVD Reactor Designed for Short-time Experiments



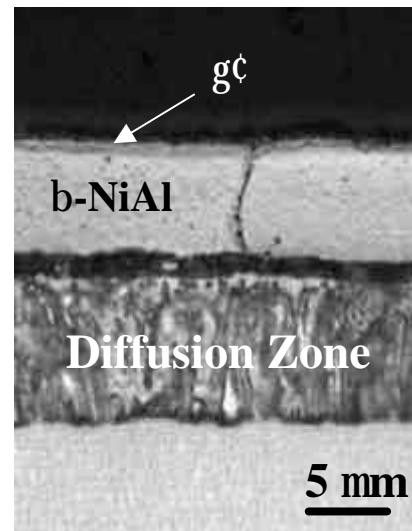
Baseline Aluminizing Behavior on René N5 (without Hf Doping)



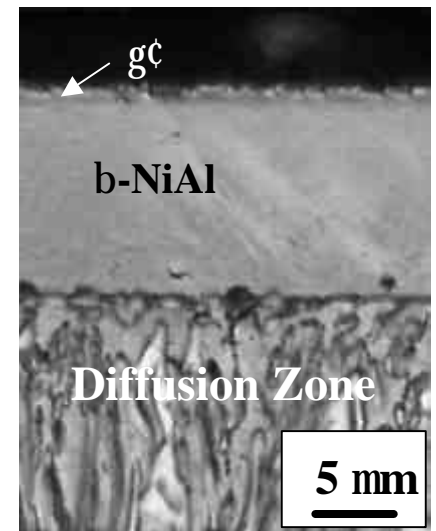
5 min



20 min

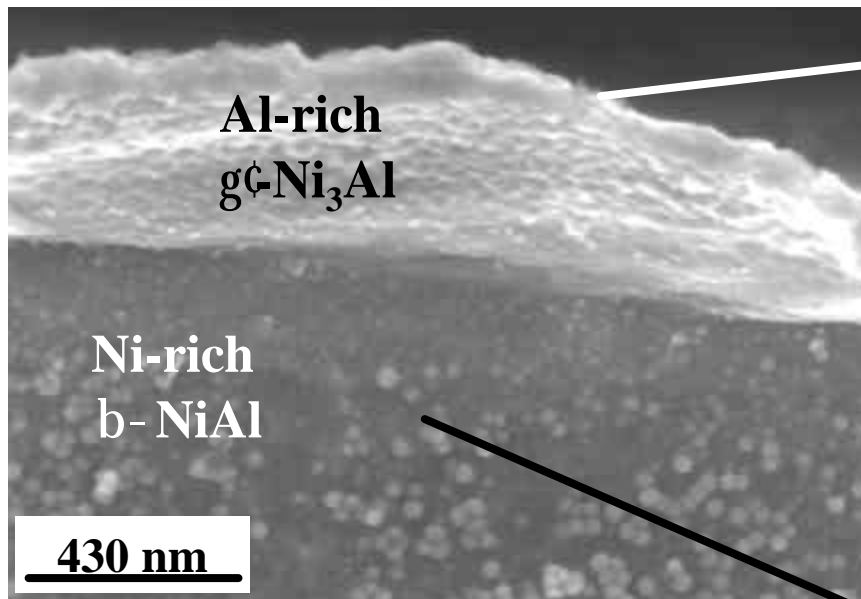


45 min

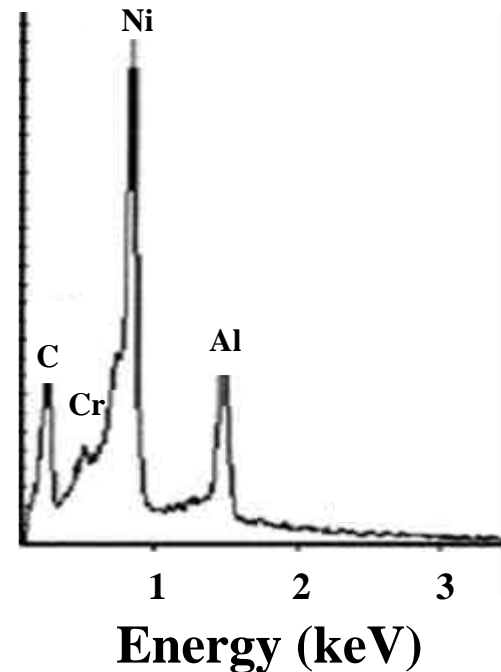
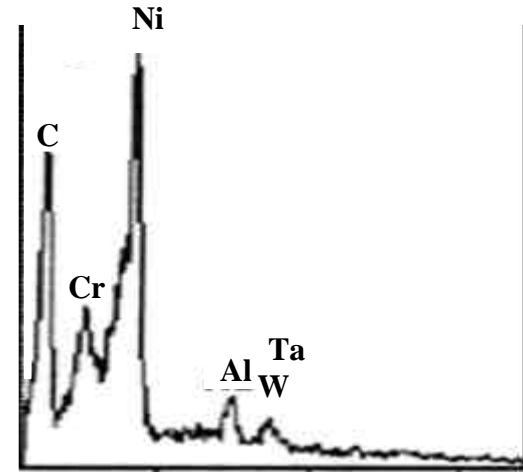


180 min

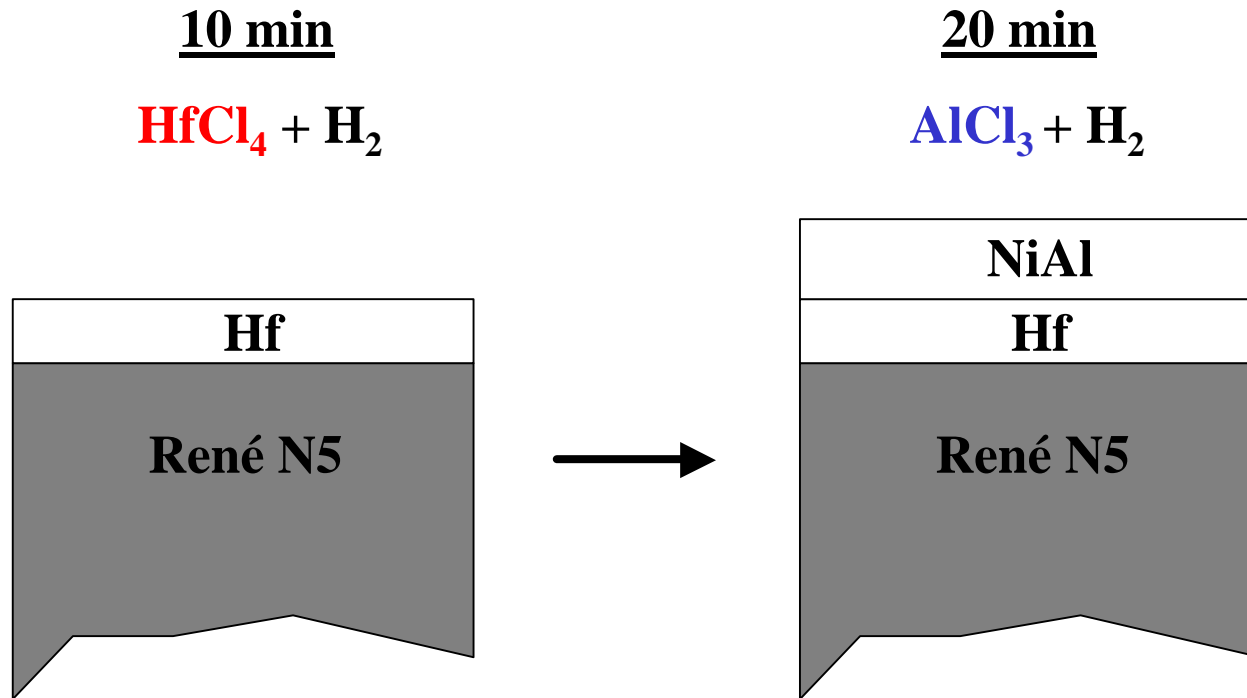
g_c Presence at Coating Surface Caused by W and Ta Segregation



After 180 min of aluminizing



First Approach: Sequential Doping Procedure

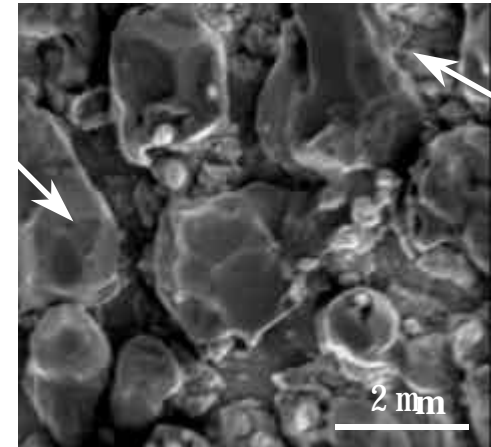
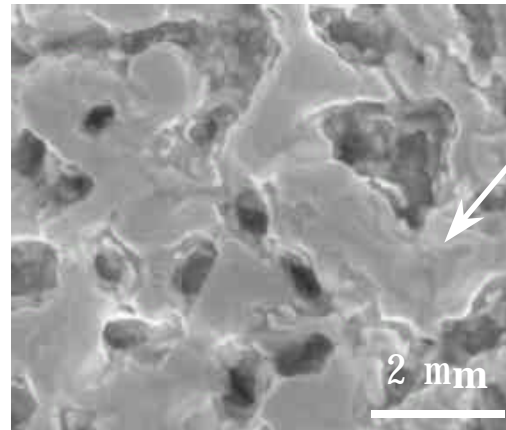
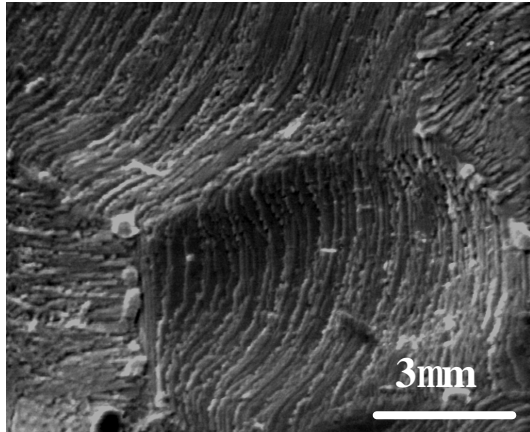


Hf-rich Precipitates Act as Ni Outward Diffusion Barrier and Retard β -NiAl Formation

20 min aluminizing

0.5 min Hf predeposition

10 min Hf predeposition



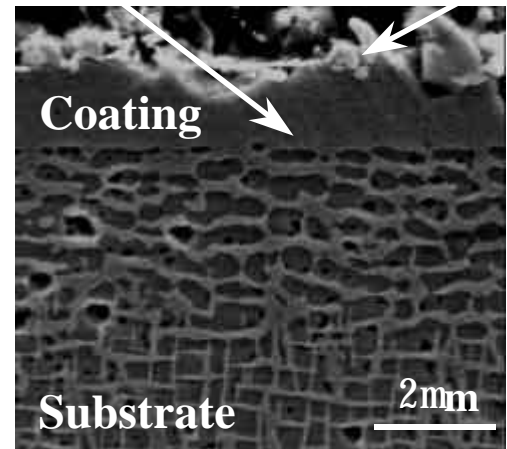
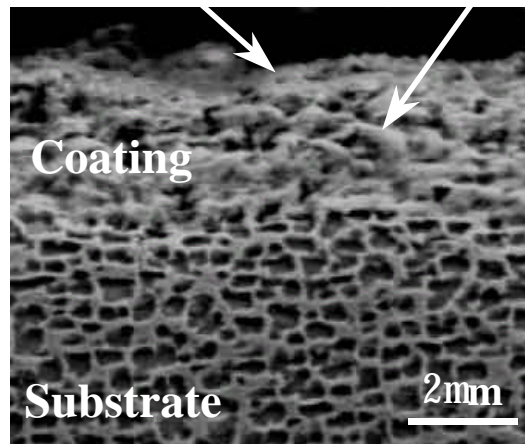
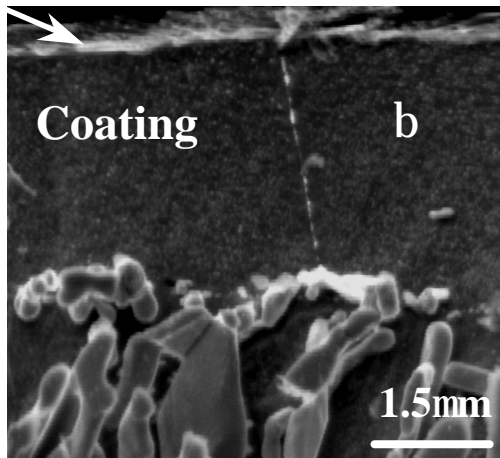
Hf ppts

$\gamma\zeta$

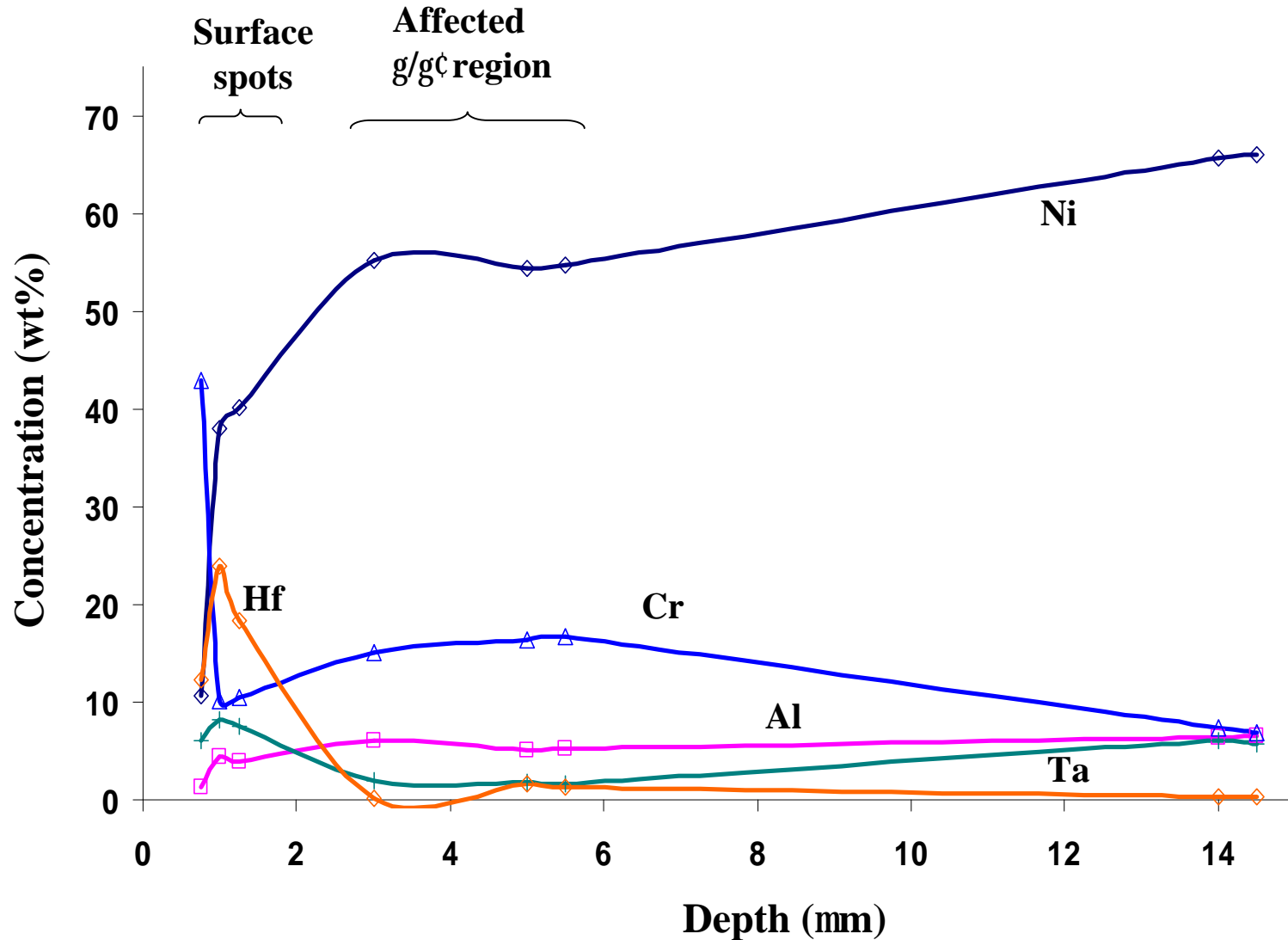
$\gamma\zeta$ +Hf ppts

β +Hf ppts

$\gamma\zeta$ +Hf ppts



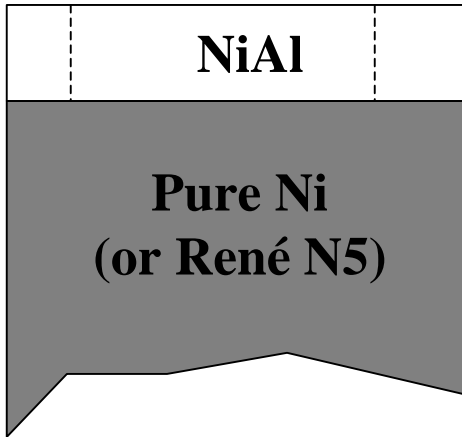
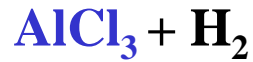
Significant Hf Incorporation by Sequential Doping



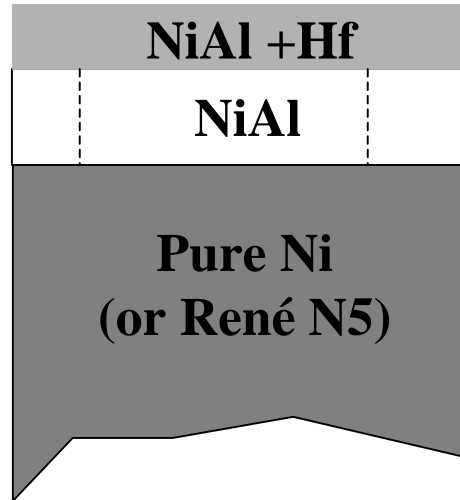
10 min Hf predeposition

Second Approach: Continuous Doping Procedure

20 min

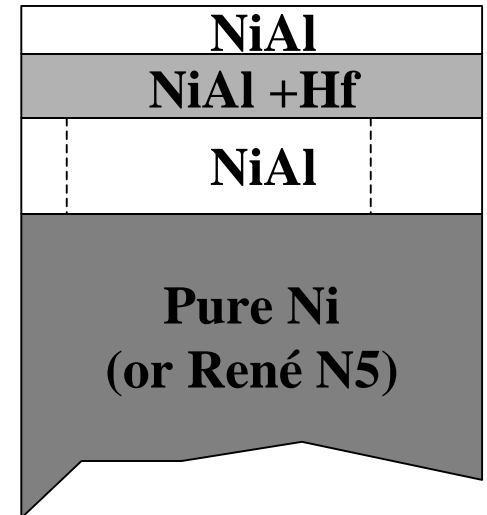
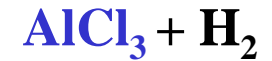


15 min



$$\left(\frac{\text{HfCl}_4}{\text{AlCl}_3} = 0.02 \sim 1.88 \right)$$

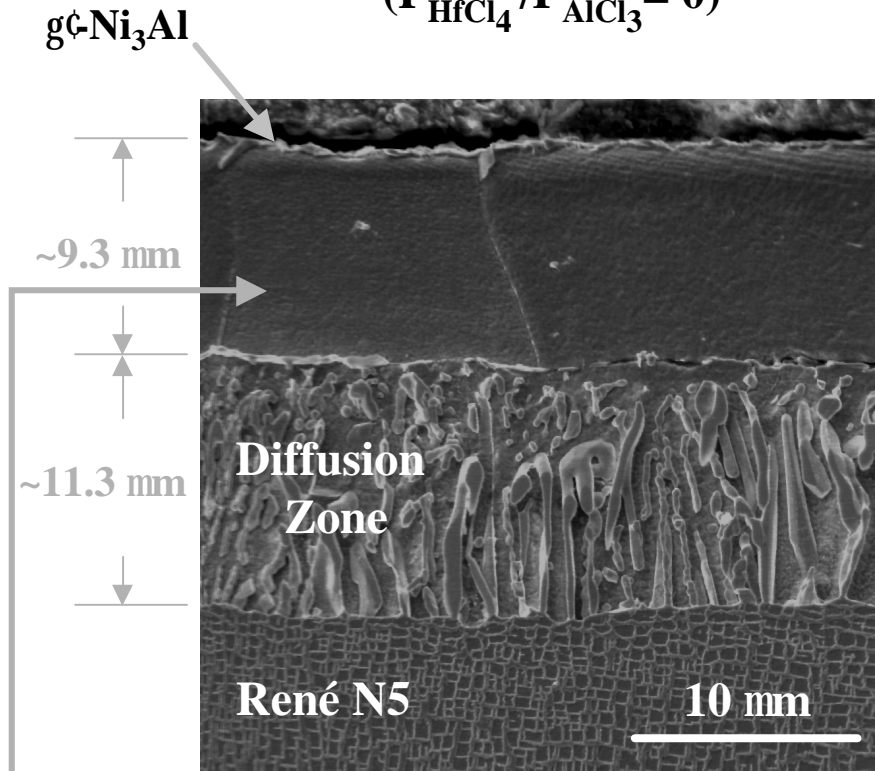
10 min



Very Low Hf Conc. Even at High HfCl₄ Conc.

Without Doping

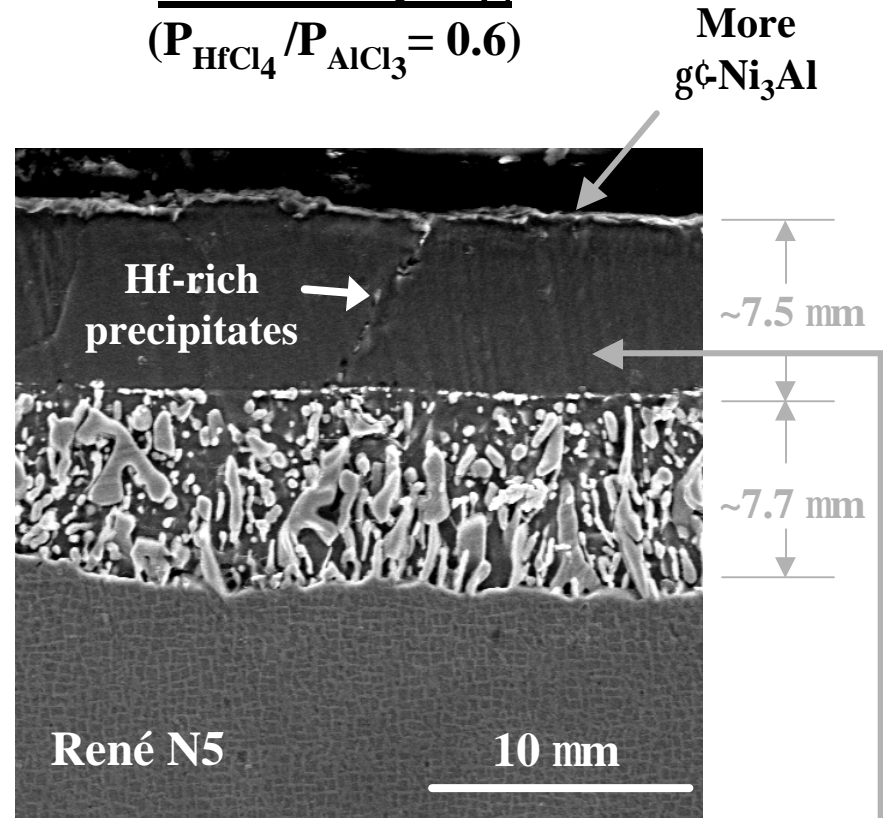
$$(P_{\text{HfCl}_4}/P_{\text{AlCl}_3} = 0)$$



~0.01 wt% Hf
(from René N5)

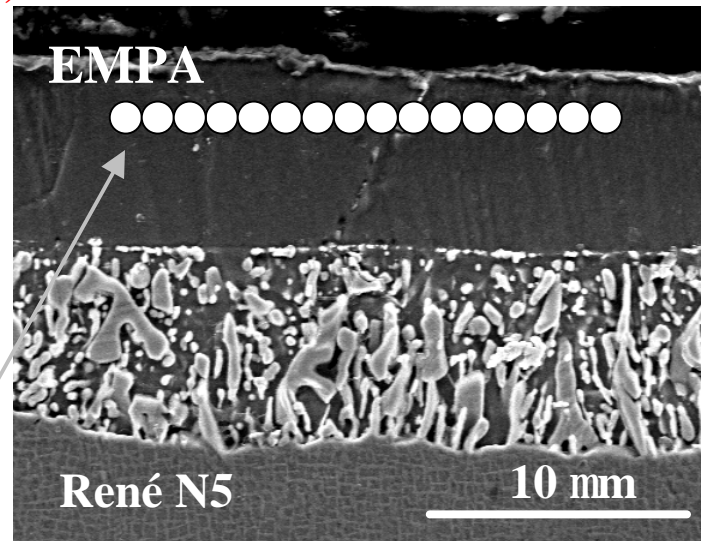
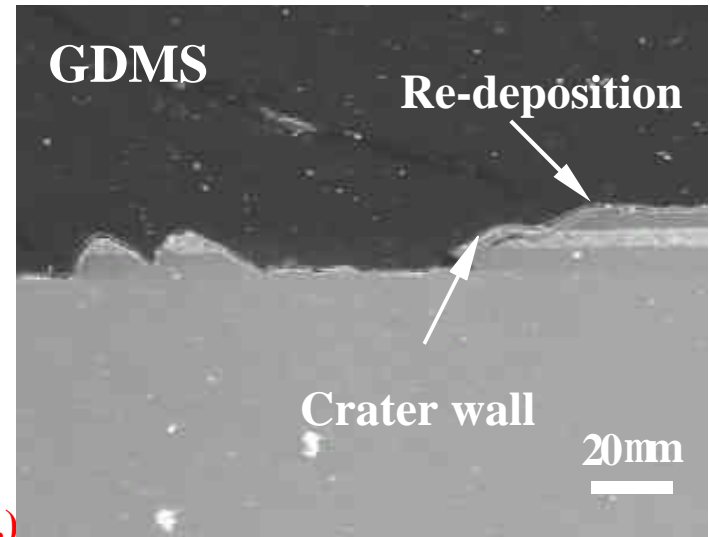
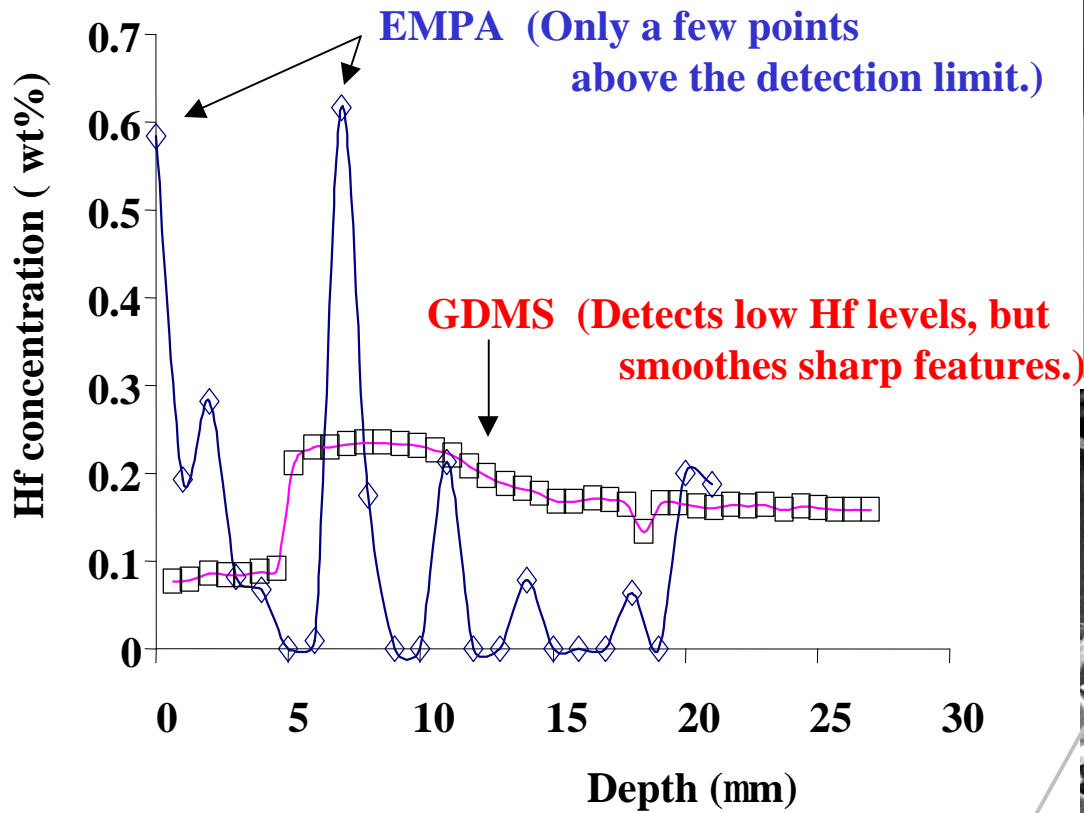
With Doping

$$(P_{\text{HfCl}_4}/P_{\text{AlCl}_3} = 0.6)$$



~0.1 wt% Hf
due to precipitates

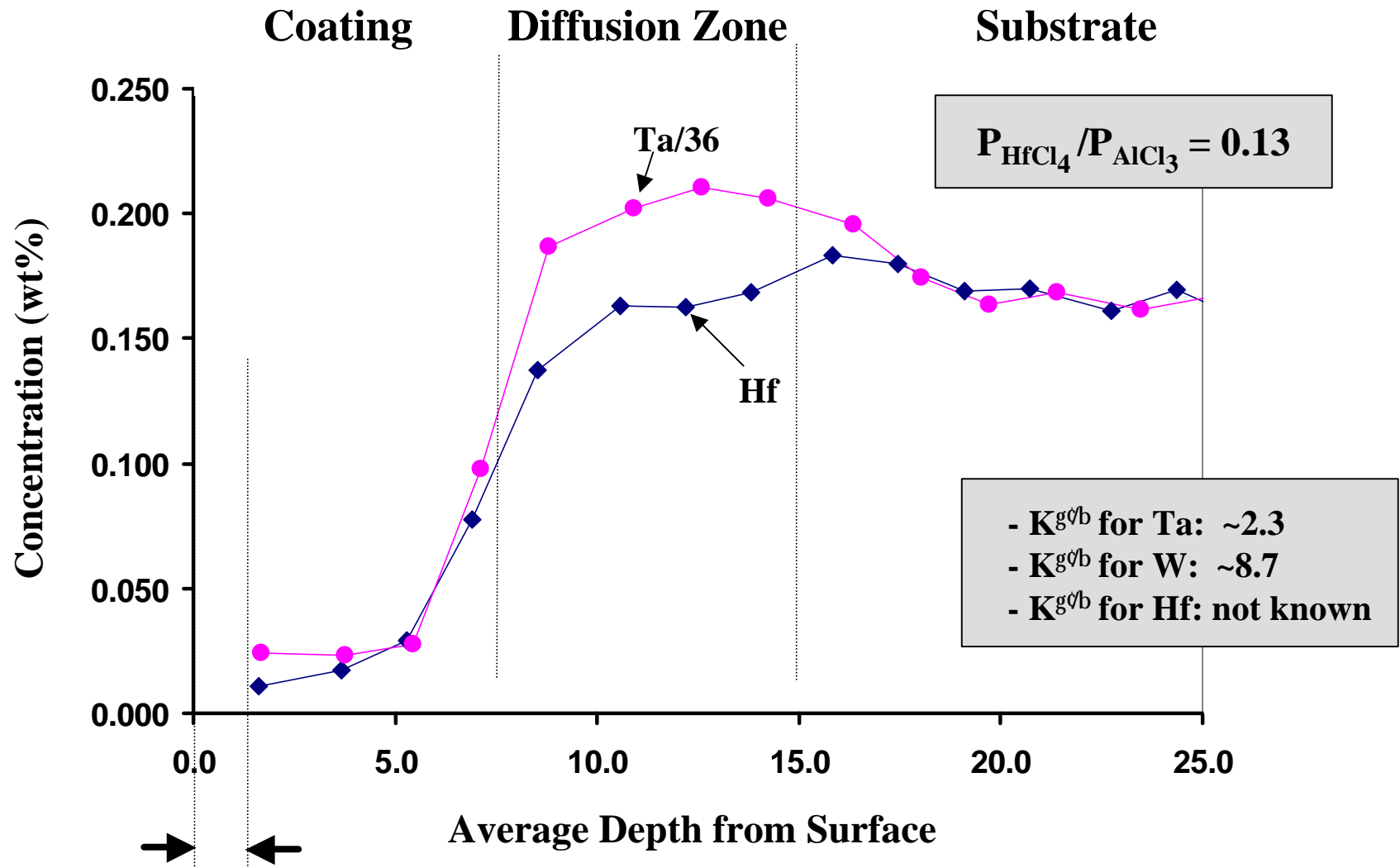
Hf Conc. And Dist. Measured by GDMS & EMPA



line scan

$$P_{\text{HfCl}_4} / P_{\text{AlCl}_3} = 0.6$$

Hf and Ta Concentration Profiles at Low HfCl_4

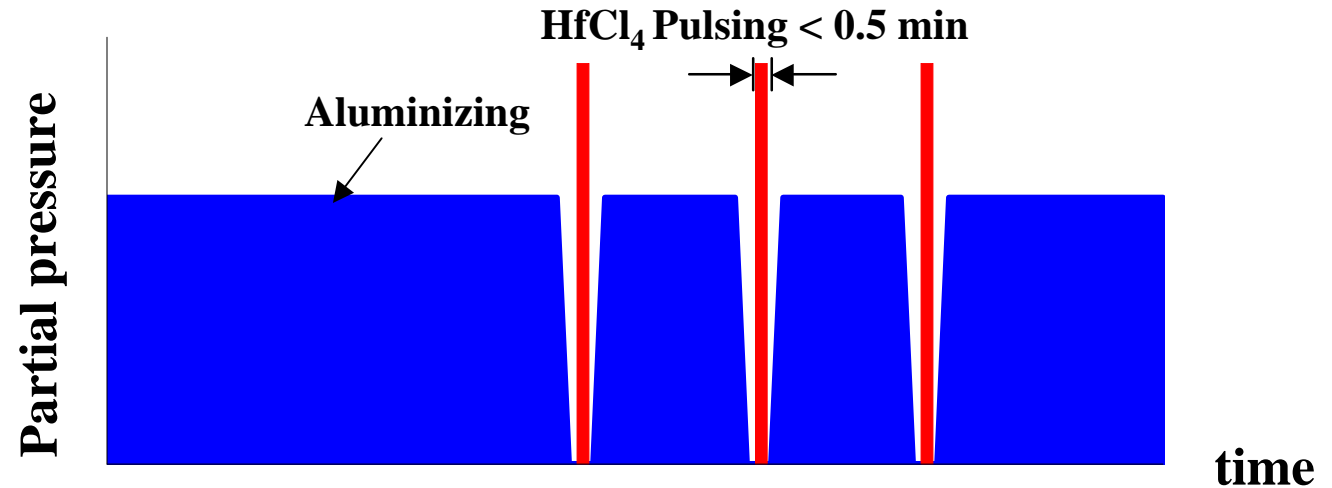


Observations During Process Development

- **Sequential Doping**
 - Significant Hf incorporation through Hf-rich precipitates
 - Hf-rich Precipitates worked as diffusion barriers and altered coating microstructure
- **Continuous Doping**
 - Retained columnar microstructure
 - Hf incorporation during continuous doping appeared to limited by its solubility in b-NiAl
 - High HfCl₄/AlCl₃ ratio were needed
- **Future Work**
 - “Floating behavior” of g_c-Ni₃Al layer at the coating surface and its effects on aluminizing kinetics and Hf incorporation behavior
 - Preparation of Hf-doped coating specimens for performance evaluation
~0.01 to 3 wt% Hf

How to Synthesize Coatings with 0.01 to 3 wt% Hf?

0.01 wt%Hf



0.10 wt%Hf

