

*Materials and Processing Issues
Associated With
Seal Coating Development*

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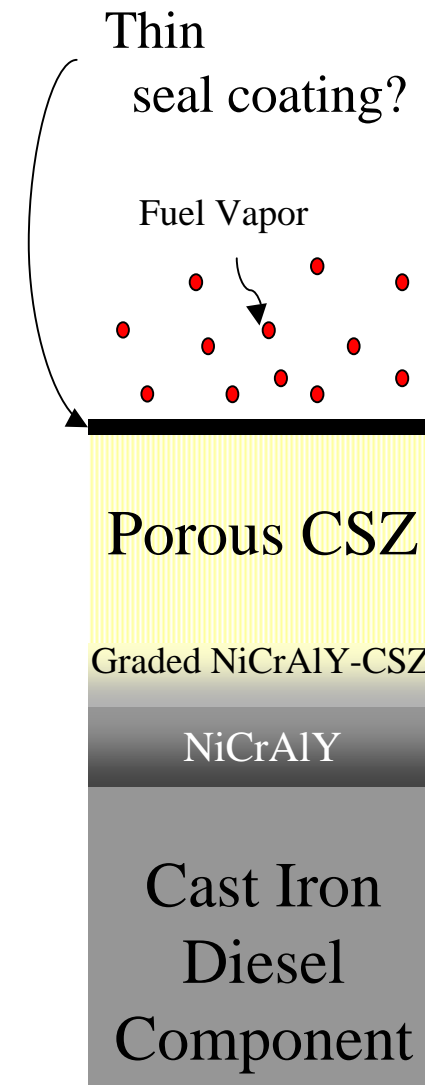
January 25, 1999

Acknowledgments

- Current research sponsored by Brad Beardsley at *Caterpillar, Inc.*
- The results from the chloride-based Al_2O_3 coating work were obtained by W.Y. Lee at Oak Ridge National Laboratory under the sponsorship of Ray Johnson, *Heavy Vehicle Propulsion System Materials Program*, DOE Office of Transportation Technologies.

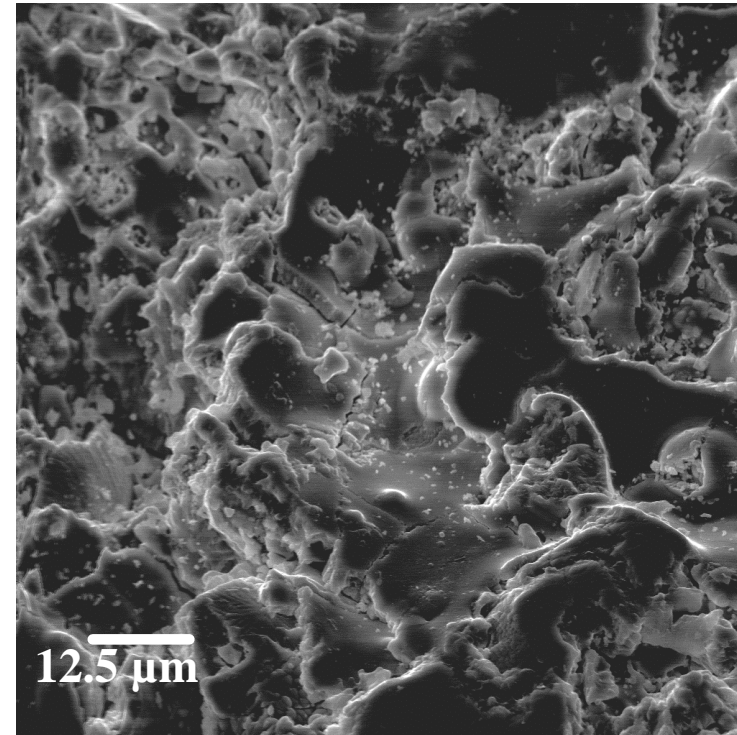
Rationale for Seal Coating

- Thermal Barrier Coatings (TBCs) are being considered to improve diesel engine efficiency
 - CeO_2 -stabilized ZrO_2 (CSZ) prepared by air plasma spray (APS) provides thermal insulation of diesel components
 - APS-CSZ is made porous for strain tolerance and enhanced thermal insulation
- Unexpectedly, testing at Caterpillar revealed a decrease in engine efficiency when components were coated with a TBC
 - One possible reason may be the porosity of the TBC, which is suspected to “entrain” fuel from the combustion chamber prior to ignition [B. Beardsley, 1990]



This Project Explores the Feasibility of Sealing the Porous TBC Surface by Applying a Seal Coating

- Materials Criteria
 - Non-porous and impermeable
 - Good adhesion to CSZ
 - High thermal stability
 - No debit to CSZ strain tolerance
 - Resistance to erosion and wear
- Processing Criteria
 - Processing temperatures below 500°C to avoid tempering of iron components
 - Conformal coating on complex, porous TBC surface



Surface morphology
of APS-CSZ
(as received)

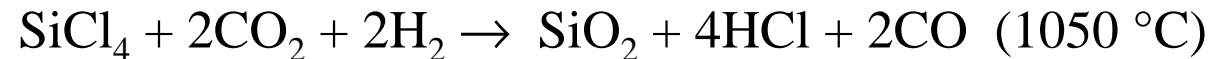
Coating Material Selection

Candidate Seal Coating Materials Were Screened Without Cast Iron Substrate

- “Free-standing” APS-CSZ coupons (1x1cm) were coated with:

MATERIAL	CTE (x10 ⁻⁶ /K)	MODULUS (GPa)
α-Al ₂ O ₃	8	380
3Al ₂ O ₃ ·2SiO ₂	6	145
SiO ₂ (fused)	0.5	70
CSZ (substrate)	~10	~200
Si (substrate)	3	163

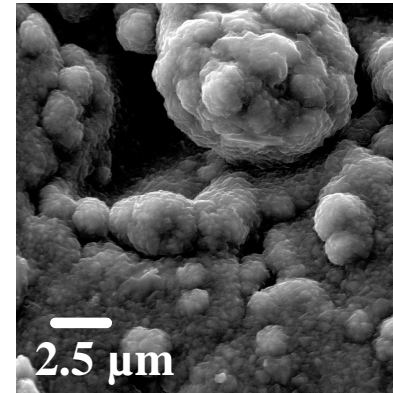
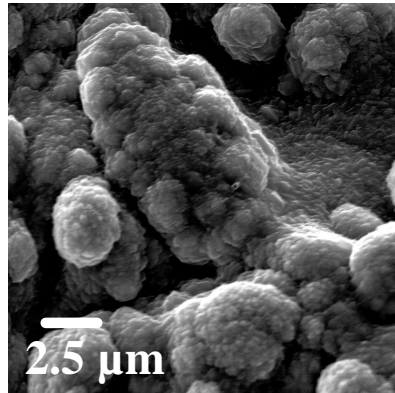
- High-temperature chloride-based CVD processes were used:



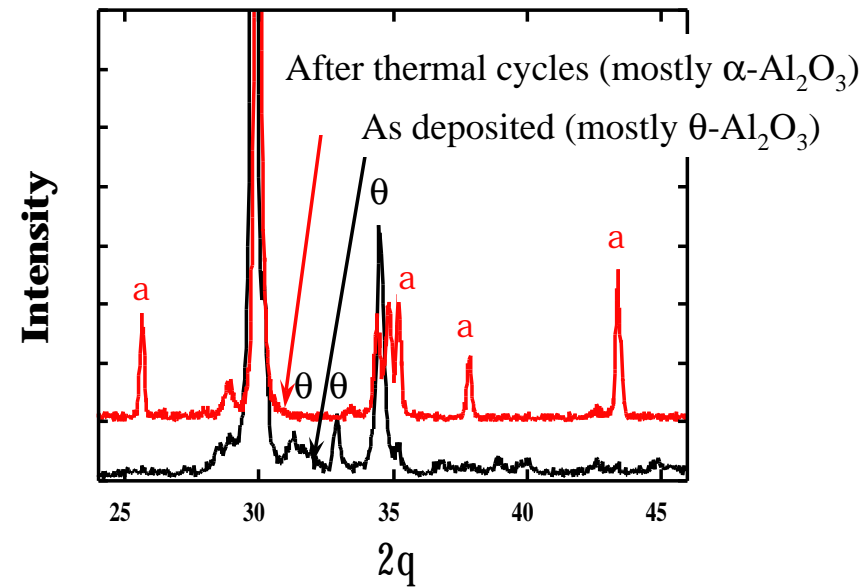
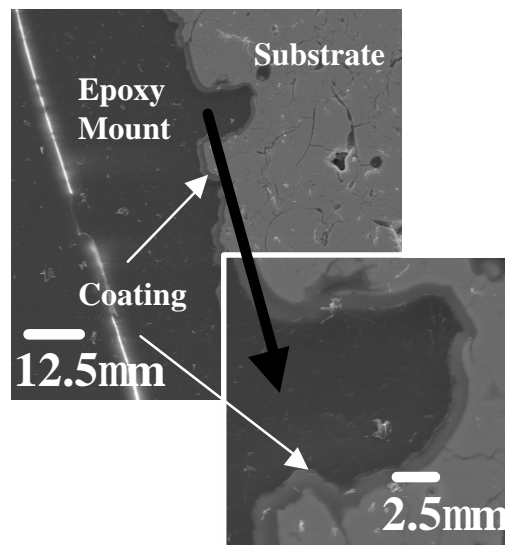
- Thermally cycled to 1150°C in air to assess seal coating/CSZ stability
- 3Al₂O₃·2SiO₂ and SiO₂ spalled during thermal cycling, probably due to CTE mismatch with respect to CSZ

Al₂O₃ Seal Coating (from Chloride Process) Was Uniform, Conformal, and Thermally Stable

As coated:



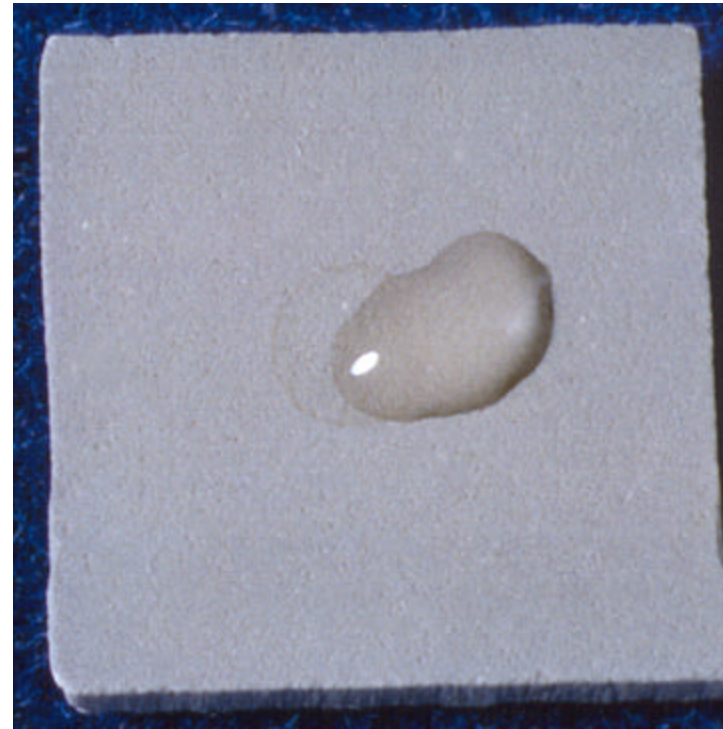
After 49
1-h. Cycles
to 1150°C.



*Screening Results Suggest That Metastable
 Al_2O_3 Seal Coating May Be Useful If It Can
Be Prepared at $T < 500^\circ C$*



Free-standing CSZ without
seal coating

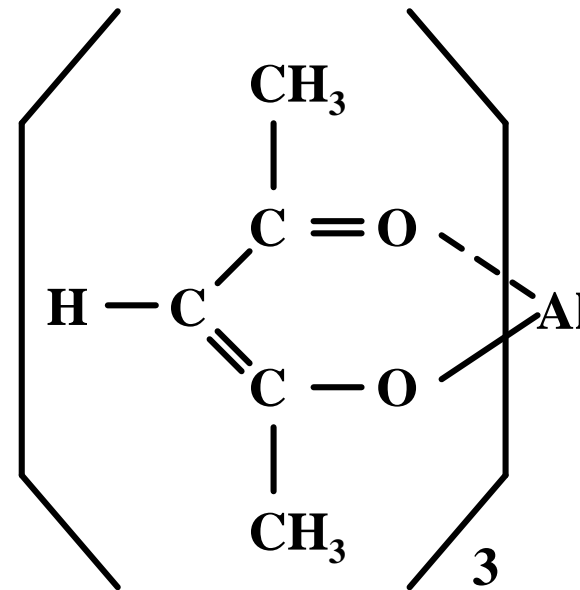


Free-standing CSZ coated
and cycled

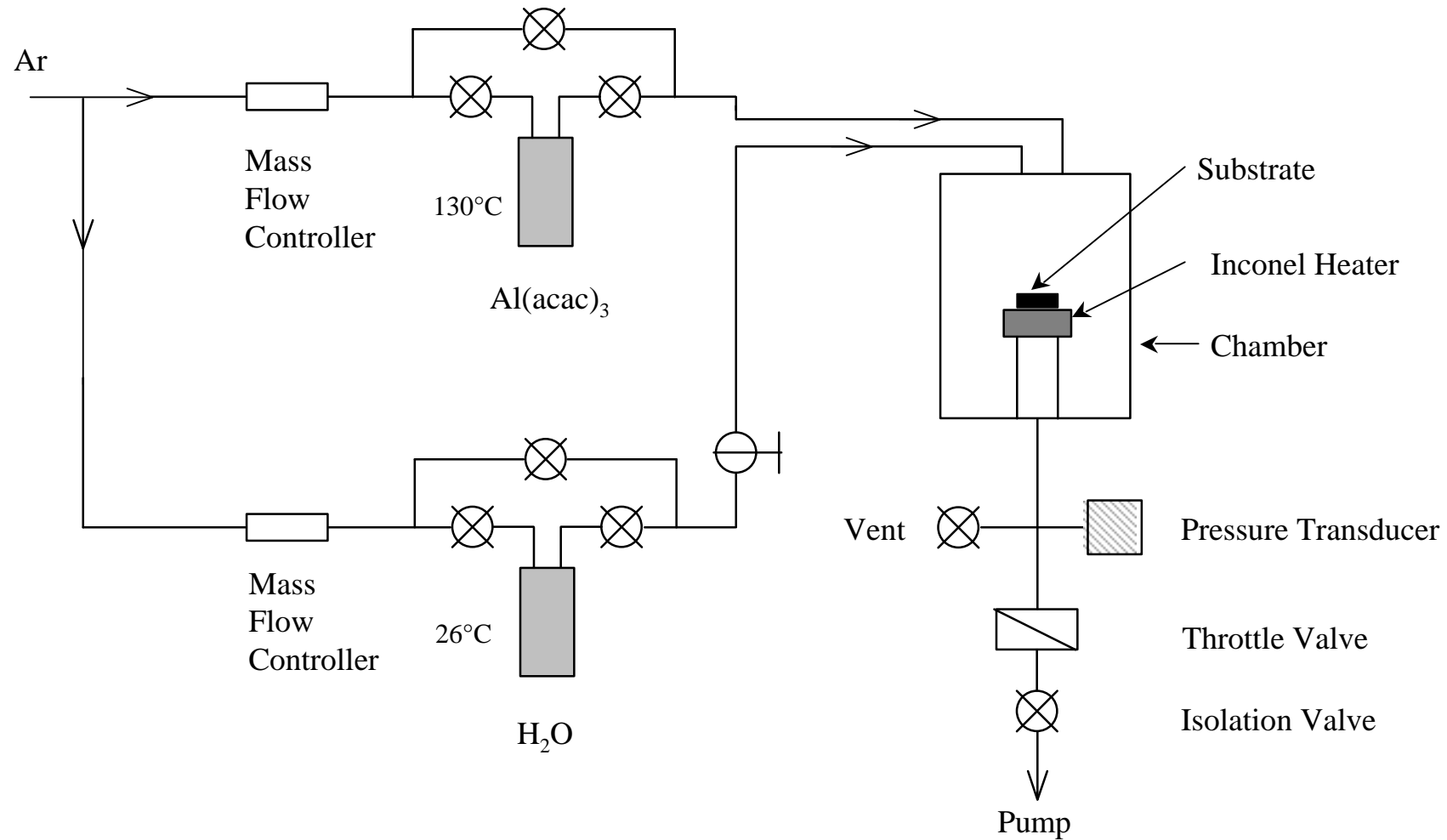
MOCVD Al₂O₃ Coating Synthesis

Al(acac)₃ and H₂O Were Selected to Prepare Low-temperature Al₂O₃ Seal Coating

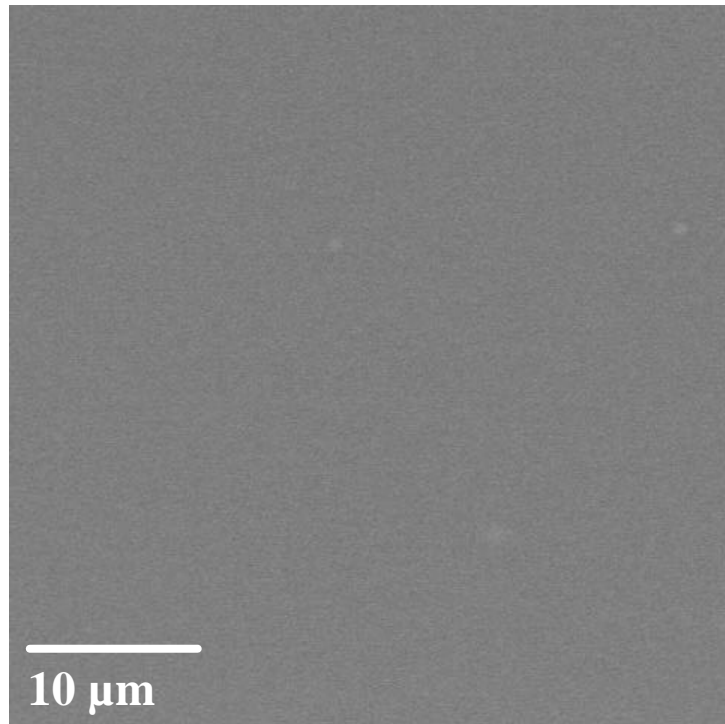
- Major reasons:
 - Decomposes readily (well below 500°C)
 - Low toxicity and cost
 - Relatively moisture-insensitive
 - Stable compound at room temperature
 - Some carbon contamination observed
- Inclusion of water vapor appears to help eliminate carbon contamination [J.S. Kim *et al.*, 1993]



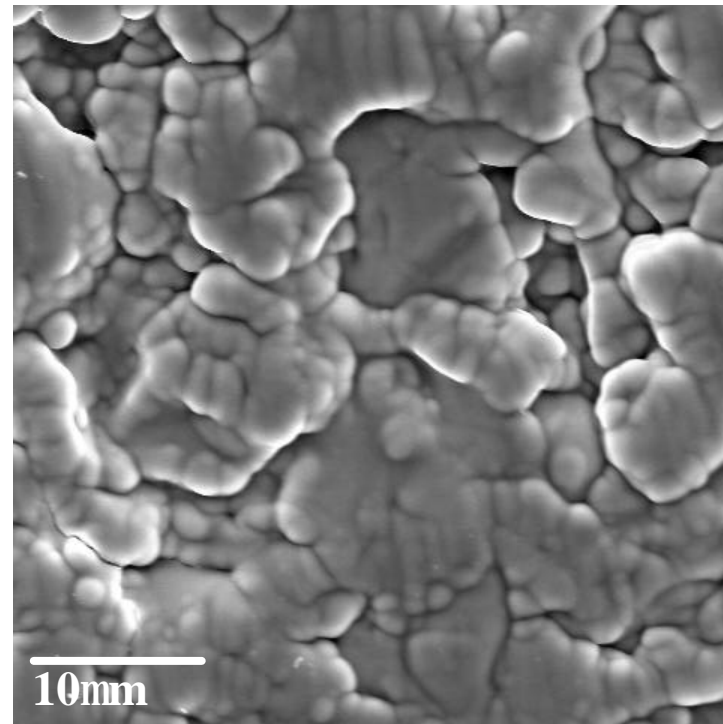
Cold-wall Al_2O_3 MOCVD System Constructed



Uniform and Conformal MOCVD Al₂O₃ Seal Coating Was Prepared at 500°C



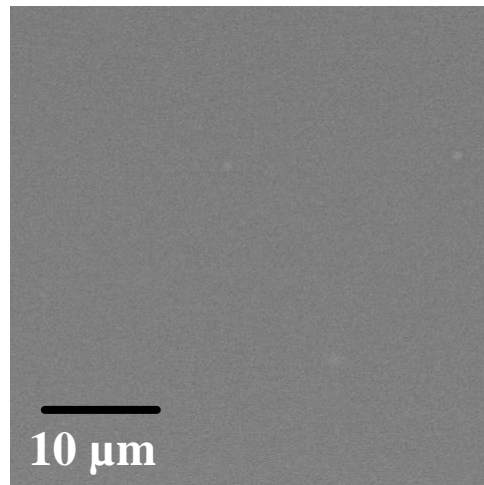
Al₂O₃ on Silicon



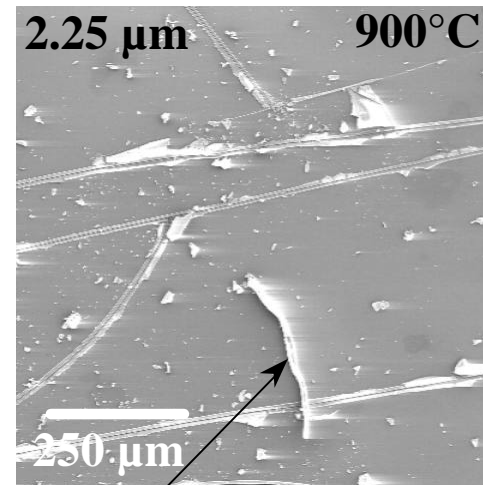
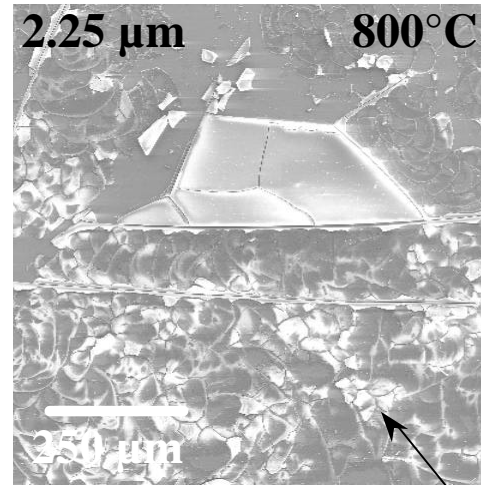
Al₂O₃ on CSZ

Thermal Stability of MOCVD Al₂O₃ Coating

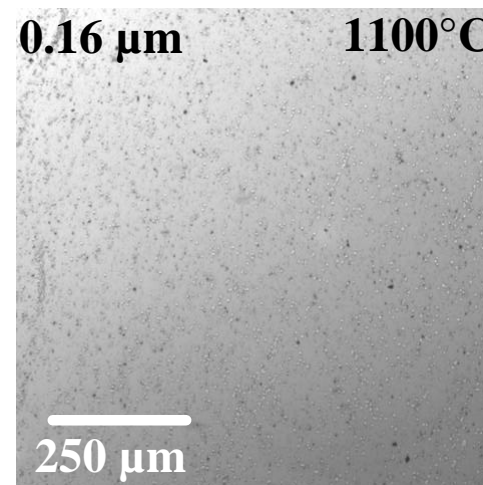
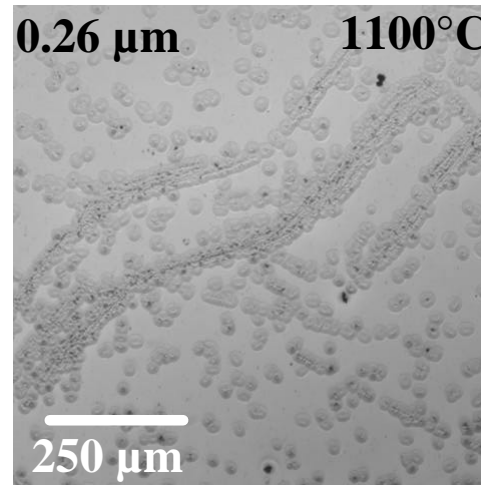
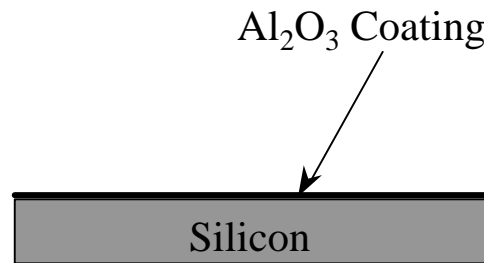
Thinner Al₂O₃ Coating on Silicon Did Not Spall upon Annealing



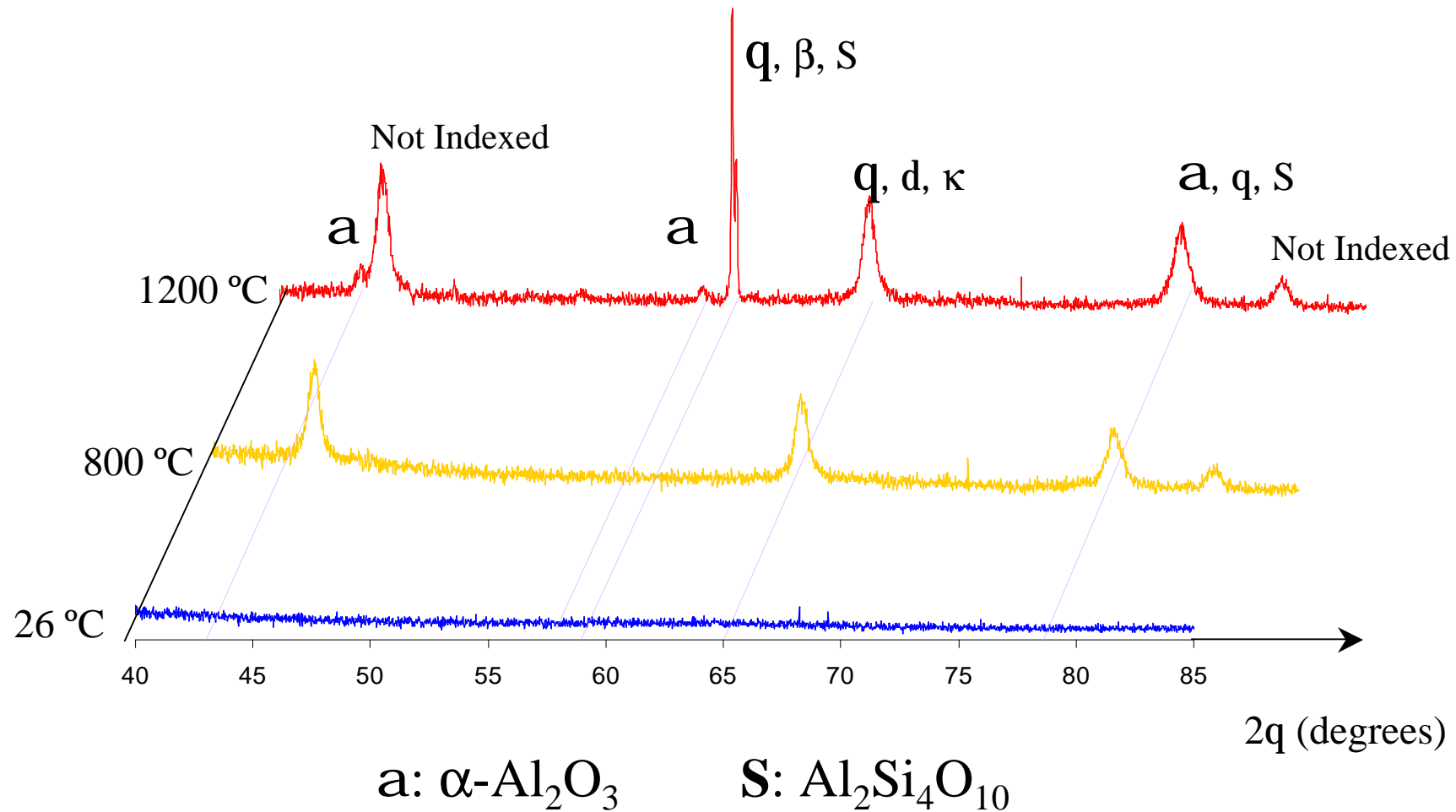
As coated



Non-spalled Al₂O₃

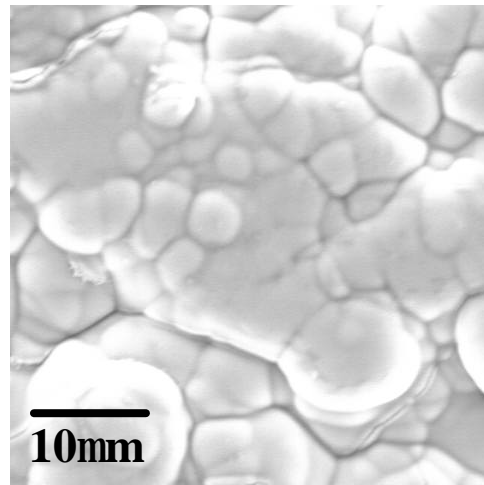


Crystallization of Al_2O_3 Occurred Relatively Rapidly (<20 Hours) at 700°C to 1200°C

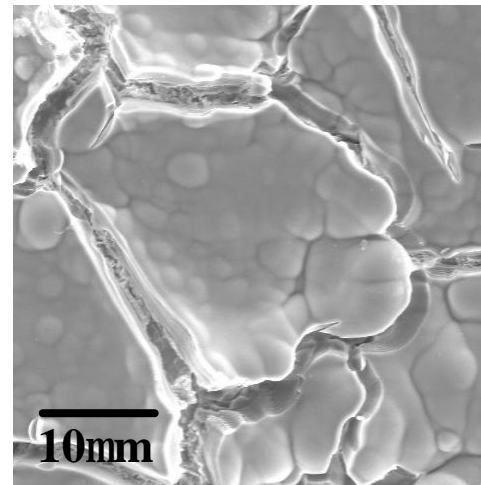


Not much Al_2O_3 remained on the substrate for XRD analysis

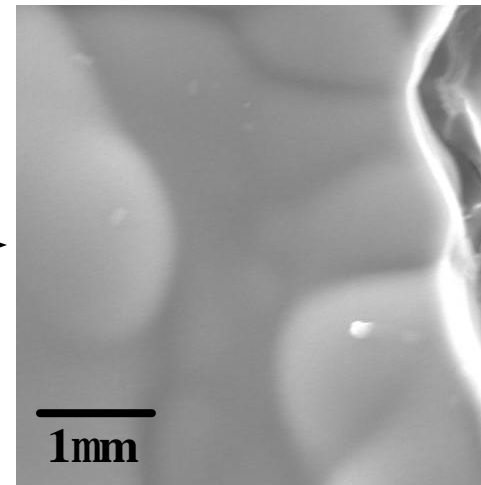
Al₂O₃ on Constrained CSZ/Iron Substrate Cracked Upon Annealing



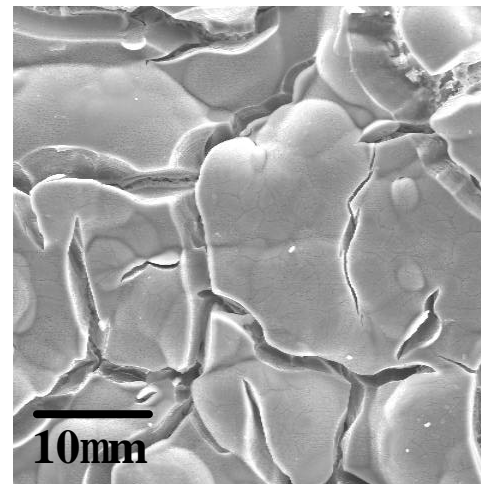
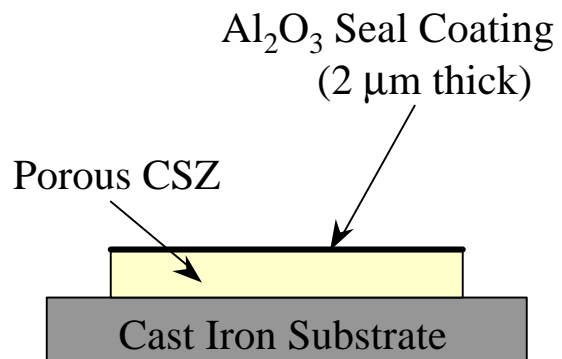
As coated



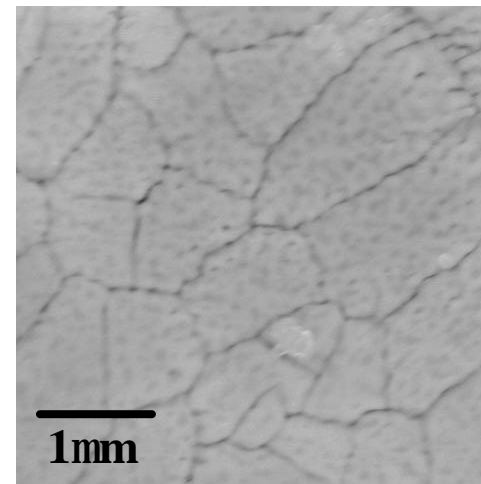
10x



900°C



10x



1000°C

Comparison & Summary

Annealing of MOCVD Al₂O₃ Leads to Inadequate Adhesion and Sealing

- Considerable spallation on silicon with 2.25 μm coating
 - CTE mismatch
 - Volume shrinkage due to crystallization (> ~9%)
- Sub-micron coatings on silicon were less susceptible to spallation
- Adhered on CSZ, but coating cracked as crystallization occurred
 - Less CTE mismatch with CSZ than with Si
 - Better adhesion may be due to mechanical interlocking at CSZ/coating interface
 - Volume shrinkage still significant (> ~ 9%)

Comparison of Chloride-based Al_2O_3 vs. MOCVD Al_2O_3

	<i>Chloride-based Al_2O_3</i>	<i>MOCVD Al_2O_3</i>
<i>As prepared:</i>	Conformal, mostly metastable (θ)	Conformal, amorphous
<i>Thermally annealed:</i>	Retained adhesion & no cracking	Severe cracking, despite adhesion
<i>Crystallization:</i>	$\theta-Al_2O_3 \rightarrow \alpha-Al_2O_3$ ($\Delta V \sim -9\%$)	Amorphous \rightarrow metastable, $\alpha-Al_2O_3$ ($\Delta V > -9\%$)
<i>Possible C & H impurities:</i>	Highly unlikely	Possible, but minimized
<i>Quality of sealing:</i>	“Sufficient”	“Insufficient”

Conclusions

- Chloride-based Al_2O_3 coating deposited at 1050°C was mostly $\theta\text{-Al}_2\text{O}_3$
 - Sealed the porous surface, although it transformed from θ - to $\alpha\text{-Al}_2\text{O}_3$
- MOCVD Al_2O_3 coating could be prepared at 500°C , but was amorphous
 - Adhered to CSZ upon annealing, but cracked extensively
- Metastable Al_2O_3 coating (*e.g.*, $\theta\text{-Al}_2\text{O}_3$) and appropriate processing modifications may be required